Appendix F: Mission Street/SR 285 Lane Assignment Memo



## **MEMORANDUM**

Date:	June 15, 2022 <b>TO</b>	<b>3</b> :	1.21200.00
То:	Riley Shewak, CDTC		
From:	Brent Turley, PE - Transpo Group		
cc:			
Subject:	Traffic Operations Analysis: Mission Street & Stevens Street Interse	ectic	n

The purpose of this memorandum is to document the traffic operations evaluation of the Mission Street/Stevens Street intersection in the southern part of Wenatchee, WA. At the request of the City of Wenatchee and CDTC, the intersection was evaluated with a slight change in channelization on the south leg of the intersection. The operations analysis and findings are presented below.

## Intersection Traffic Operations

The future traffic volume forecasts for the Mission Street/Stevens Street intersection were developed as part of CDTC's *South Wenatchee Connectivity Study* (Transpo Group, June 2022). These forecasts represent weekday PM peak hour volumes during the 2045 horizon year.

The 2045 Baseline scenario represents 2045 conditions with existing lane configurations at the study intersection. On the northbound approach, this Baseline scenario has one northbound through lane and two northbound right-turn lanes. The Alternative scenario **converts the center lane to a shared through-right-turn lane**.

PM peak hour traffic operations were evaluated at the study intersections based on level of service (LOS). The LOS analysis method was based on procedures identified in the *Highway Capacity Manual* (6th Edition), and evaluated using Synchro version 11.0.

At signalized intersections, LOS is measured in average control delay per vehicle and is typically reported using the intersection delay. Traffic operations for an intersection can be described alphabetically with a range of levels of service (LOS A through F), with LOS A indicating free-flowing traffic and LOS F indicating extreme congestion and long vehicle delays. The City of Wenatchee has established LOS E as the LOS standard for city street intersections and WSDOT uses LOS D as its standard for state highway intersections. The study intersection is a state highway intersection. Table 1 summarizes the weekday PM peak hour LOS at study intersections. The detailed LOS worksheets are included in as attachments.

Table 1. Intersection LOS Sum	Intersection LOS Summary - PM Peak Hour									
	2045 B	aseline	2045 Alternative <sup>3</sup>							
	LOS <sup>1</sup>	Delay <sup>2</sup>	LOS	Delay						
Mission Street/ Stevens Street	D	43.7	Е	56.0						
Source: Transpa Croup 2022										

Source: Transpo Group, 2022

1. Level of Service (LOS), based on Highway Capacity Manual (6th Edition) methodology.

2. Average delay in seconds per vehicle.

. The Alternative Scenario is based on the 2000 Highway Capacity Manual due to the unusual south leg channelization.

## Findings

As shown in Table 1, the Alternative scenario would degrade traffic operations from LOS D to LOS E. This is primarily due to the removal of the northbound right-turn overlap signal phase which runs concurrent with the westbound left-turn phase. In the Alternative scenario, this phase would not be allowed, so right-turning traffic would need to come to a stop before proceeding to turn-on-red. This reduced capacity for the northbound right-turn movements increases overall average signal delay to an unacceptable level. The Alternative scenario northbound-through movements do have more capacity compared to the Baseline scenario, but northbound-through traffic volumes are only 30% of the northbound right-turn traffic volume level. The existing lane configuration appears to provide the best available capacity to the movements in most need of the capacity.

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Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	ሻሻ	11	•	11	ካካ	*		
Traffic Volume (veh/h)	610	1240	220	720	1980	350		
Future Volume (veh/h)	610	1240	220	720	1980	350		
Initial Q (Qb), veh	0	0	0	0	0	0		
Ped-Bike Adj(A_pbT)	1.00	1.00		1.00	1.00			
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00		
Work Zone On Approach	No		No			No		
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870		
Adj Flow Rate, veh/h	656	1333	237	774	2129	376		
Peak Hour Factor	0.93	0.93	0.93	0.93	0.93	0.93		
Percent Heavy Veh, %	2	2	2	2	2	2		
Cap, veh/h	581	2067	255	850	1979	1403		
Arrive On Green	0.17	0.17	0.14	0.14	0.96	1.00		
Sat Flow, veh/h	3456	2790	1870	2790	3456	1870		
Grp Volume(v), veh/h	656	1333	237	774	2129	376		
Grp Sat Flow(s),veh/h/ln	1728	1395	1870	1395	1728	1870		
Q Serve(g_s), s	18.5	0.0	13.8	7.4	63.0	0.0		
Cycle Q Clear(g_c), s	18.5	0.0	13.8	7.4	63.0	0.0		
Prop In Lane	1.00	1.00	_	1.00	1.00			
Lane Grp Cap(c), veh/h	581	2067	255	850	1979	1403		
V/C Ratio(X)	1.13	0.64	0.93	0.91	1.08	0.27		
Avail Cap(c_a), veh/h	581	2067	255	850	1979	1403		
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.67	1.67		
Upstream Filter(I)	1.00	1.00	1.00	1.00	0.73	0.73		
Unitorm Delay (d), s/veh	45.8	7.1	47.0	28.7	2.4	0.0		
Incr Delay (d2), s/veh	/8.1	0.7	40.7	15.6	41.8	0.3		
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0		
%IIE BACKUTQ(50%), veh/In	14.2	6.6	9.3	11.3	12.6	0.1		
Unsig. Movement Delay, s/veh	102.0	7.0	077	14.2	14.0	0.2		
Lingrp Delay(d),s/ven	123.8	٥./ ۸	δ/./ Γ	44.3	44.2	0.3		
	1000	A		U	F	A		
Approach Vol, veh/h	1989		1011			2505		
Approach Delay, S/Ven	40.0		54.4			37.0		
Approach LUS	D		D			D		
Timer - Assigned Phs	1	2				6	8	
Phs Duration (G+Y+Rc), s	67.5	19.5				87.0	23.0	
Change Period (Y+Rc), s	4.5	4.5				4.5	4.5	
Max Green Setting (Gmax), s	63.0	15.0				82.5	18.5	
Max Q Clear Time (g_c+I1), s	65.0	15.8				2.0	20.5	
Green Ext Time (p_c), s	0.0	0.0				2.6	0.0	
Intersection Summary								
HCM 6th Ctrl Delay			43.7					
HCM 6th LOS			D					

WBL <b>11</b> 610 610	WBR	NBT	NBR	SBI	CDT			
<b>ካካ</b> 610 610	11			ODL	301			
610 610		- <b>1</b> 16	1	ሻሻ	•			
610	1240	220	720	1980	350			
010	1240	220	720	1980	350			
1900	1900	1900	1900	1900	1900			
4.5	4.5	4.5	4.5	4.5	4.5			
0.97	0.88	0.91	0.91	0.97	1.00			
1.00	0.85	0.91	0.85	1.00	1.00			
0.95	1.00	1.00	1.00	0.95	1.00			
3433	2787	3075	1441	3433	1863			
0.95	1.00	1.00	1.00	0.95	1.00			
3433	2787	3075	1441	3433	1863			
0.93	0.93	0.93	0.93	0.93	0.93			
656	1333	237	774	2129	376			
0	42	219	219	0	0			
656	1291	406	169	2129	376			
Prot	pt+ov	NA	Perm	Prot	NA			
3	31	2		1	6			
, ,	•	_	2	•	•			
18.5	86.0	15.0	15.0	63.0	82.5			
18.5	86.0	15.0	15.0	63.0	82.5			
0.17	0.78	0.14	0.14	0.57	0.75			
4.5		4.5	4.5	4.5	4.5			
3.0		3.0	3.0	3.0	3.0			
577	2178	419	196	1966	1397			
c0.19	0.46	c0.13		c0.62	0.20			
			0.12					
1.14	0.59	0.97	0.86	1.08	0.27			
45.8	4.9	47.3	46.5	23.5	4.3			
1.00	1.00	1.00	1.00	0.72	0.69			
81.3	0.4	36.6	35.9	45.2	0.4			
127.0	5.3	83.9	82.4	62.2	3.3			
F	А	F	F	Е	А			
45.5		83.3			53.4			
D		F			D			
HCM 2000 Control Delay		56.0	H	CM 2000	Level of Servic	9	Е	
HCM 2000 Volume to Capacity ratio		1.08						
Actuated Cycle Length (s)		110.0	Si	um of lost	time (s)		13.5	
Intersection Capacity Utilization		98.9%	IC	U Level o	of Service		F	
Analysis Period (min)		15						
	610 1900 4.5 0.97 1.00 0.95 3433 0.93 656 0 656 0 656 Prot 3 18.5 18.5 0.17 4.5 3.0 577 c0.19 1.14 45.8 1.00 81.3 127.0 F 45.5 D ratio	610  1240    1900  1900    4.5  4.5    0.97  0.88    1.00  0.85    0.95  1.00    3433  2787    0.95  1.00    3433  2787    0.93  0.93    656  1333    0  42    656  1291    Prot  pt+ov    3  31    18.5  86.0    0.17  0.78    4.5  3.0    577  2178    c0.19  0.46    1.14  0.59    45.8  4.9    1.00  1.00    81.3  0.4    127.0  5.3    F  A    45.5  D    ratio	610    1240    220      1900    1900    1900      4.5    4.5    4.5      0.97    0.88    0.91      1.00    0.85    0.91      0.95    1.00    1.00      3433    2787    3075      0.95    1.00    1.00      3433    2787    3075      0.95    1.00    1.00      3433    2787    3075      0.93    0.93    0.93      656    1333    237      0    42    219      656    1291    406      Prot    pt+ov    NA      3    3    1      0    42    219      656    1291    406      Prot    pt+ov    NA      3    3    1      18.5    86.0    15.0      18.5    86.0    15.0      0.17    0.78    0.14      4.5    4.5 </td <td>610    1240    220    720      1900    1900    1900    1900      4.5    4.5    4.5    4.5      0.97    0.88    0.91    0.91      1.00    0.85    0.91    0.85      0.95    1.00    1.00    1.00      3433    2787    3075    1441      0.95    1.00    1.00    1.00      3433    2787    3075    1441      0.95    1.00    1.00    1.00      3433    2787    3075    1441      0.93    0.93    0.93    0.93      656    1333    237    774      0    42    219    219      656    1291    406    169      Prot    pt+ov    NA    Perm      3    3.1    2    2      18.5    86.0    15.0    15.0      0.17    0.78    0.14    0.14      4.5</td> <td>610    1240    220    720    1980      1900    1900    1900    1900    1900      4.5    4.5    4.5    4.5    4.5      0.97    0.88    0.91    0.91    0.97      1.00    0.85    0.91    0.85    1.00      0.95    1.00    1.00    1.00    0.95      3433    2787    3075    1441    3433      0.95    1.00    1.00    1.00    0.95      3433    2787    3075    1441    3433      0.93    0.93    0.93    0.93    0.93      656    1333    237    774    2129      0    42    219    219    0      656    1291    406    169    2129      Prot    pt+ov    NA    Perm    Prot      3    3    1    2    1      2    1    0.50    63.0      0.17    0.78</td> <td>610  1240  220  720  1980  350    1900  1900  1900  1900  1900  1900    4.5  4.5  4.5  4.5  4.5  4.5    0.97  0.88  0.91  0.91  0.97  1.00    1.00  0.85  0.91  0.85  1.00  1.00    0.95  1.00  1.00  0.95  1.00    3433  2787  3075  1441  3433  1863    0.95  1.00  1.00  1.00  0.95  1.00    3433  2787  3075  1441  3433  1863    0.95  1.00  1.00  1.00  0.95  1.00    3433  2787  3075  1441  3433  1863    0.93  0.93  0.93  0.93  0.93  0.93    0  42  219  219  0  0    656  1291  406  169  2129  376    Prot  pt+ov  NA  Perm  Prot  NA</td> <td>610  1240  220  720  1980  350    1900  1900  1900  1900  1900  1900    4.5  4.5  4.5  4.5  4.5  4.5    0.97  0.88  0.91  0.97  1.00    1.00  0.85  0.91  0.95  1.00    3433  2787  3075  1441  3433  1863    0.95  1.00  1.00  0.95  1.00  3433  1863    0.93  0.93  0.93  0.93  0.93  0.93  0.93    0.42  219  219  0  0  656  1291  406  169  2129  376    0  42  219  219  0  0  656  1291  406  169  2129  376    Prot  pt+ov  NA  Perm  Prot  NA  3  1  2  1  6    1.5  86.0  15.0  15.0  63.0  82.5  1  1  1  1  0  1  0</td> <td>610  1240  220  720  1980  350    1900  1900  1900  1900  1900  1900    4.5  4.5  4.5  4.5  4.5  0.97    0.97  0.88  0.91  0.97  1.00  1.00    1.00  0.85  0.91  0.97  1.00    3433  2787  3075  1441  3433  1863    0.93  0.93  0.93  0.93  0.93  0.93    0.93  0.93  0.93  0.93  0.93  0.93    0.93  0.93  0.93  0.93  0.93  0.93    0.93  0.93  0.93  0.93  0.93  0.93    0.42  219  219  0  0  656    1291  406  169  2129  376    Prot  pt+ov  NA  Perm  Prot  NA    3  3.1  2  1  6    2  1  6  150  63.0  82.5    18.5  86.0</td>	610    1240    220    720      1900    1900    1900    1900      4.5    4.5    4.5    4.5      0.97    0.88    0.91    0.91      1.00    0.85    0.91    0.85      0.95    1.00    1.00    1.00      3433    2787    3075    1441      0.95    1.00    1.00    1.00      3433    2787    3075    1441      0.95    1.00    1.00    1.00      3433    2787    3075    1441      0.93    0.93    0.93    0.93      656    1333    237    774      0    42    219    219      656    1291    406    169      Prot    pt+ov    NA    Perm      3    3.1    2    2      18.5    86.0    15.0    15.0      0.17    0.78    0.14    0.14      4.5	610    1240    220    720    1980      1900    1900    1900    1900    1900      4.5    4.5    4.5    4.5    4.5      0.97    0.88    0.91    0.91    0.97      1.00    0.85    0.91    0.85    1.00      0.95    1.00    1.00    1.00    0.95      3433    2787    3075    1441    3433      0.95    1.00    1.00    1.00    0.95      3433    2787    3075    1441    3433      0.93    0.93    0.93    0.93    0.93      656    1333    237    774    2129      0    42    219    219    0      656    1291    406    169    2129      Prot    pt+ov    NA    Perm    Prot      3    3    1    2    1      2    1    0.50    63.0      0.17    0.78	610  1240  220  720  1980  350    1900  1900  1900  1900  1900  1900    4.5  4.5  4.5  4.5  4.5  4.5    0.97  0.88  0.91  0.91  0.97  1.00    1.00  0.85  0.91  0.85  1.00  1.00    0.95  1.00  1.00  0.95  1.00    3433  2787  3075  1441  3433  1863    0.95  1.00  1.00  1.00  0.95  1.00    3433  2787  3075  1441  3433  1863    0.95  1.00  1.00  1.00  0.95  1.00    3433  2787  3075  1441  3433  1863    0.93  0.93  0.93  0.93  0.93  0.93    0  42  219  219  0  0    656  1291  406  169  2129  376    Prot  pt+ov  NA  Perm  Prot  NA	610  1240  220  720  1980  350    1900  1900  1900  1900  1900  1900    4.5  4.5  4.5  4.5  4.5  4.5    0.97  0.88  0.91  0.97  1.00    1.00  0.85  0.91  0.95  1.00    3433  2787  3075  1441  3433  1863    0.95  1.00  1.00  0.95  1.00  3433  1863    0.93  0.93  0.93  0.93  0.93  0.93  0.93    0.42  219  219  0  0  656  1291  406  169  2129  376    0  42  219  219  0  0  656  1291  406  169  2129  376    Prot  pt+ov  NA  Perm  Prot  NA  3  1  2  1  6    1.5  86.0  15.0  15.0  63.0  82.5  1  1  1  1  0  1  0	610  1240  220  720  1980  350    1900  1900  1900  1900  1900  1900    4.5  4.5  4.5  4.5  4.5  0.97    0.97  0.88  0.91  0.97  1.00  1.00    1.00  0.85  0.91  0.97  1.00    3433  2787  3075  1441  3433  1863    0.93  0.93  0.93  0.93  0.93  0.93    0.93  0.93  0.93  0.93  0.93  0.93    0.93  0.93  0.93  0.93  0.93  0.93    0.93  0.93  0.93  0.93  0.93  0.93    0.42  219  219  0  0  656    1291  406  169  2129  376    Prot  pt+ov  NA  Perm  Prot  NA    3  3.1  2  1  6    2  1  6  150  63.0  82.5    18.5  86.0

c Critical Lane Group